



Jun *30, 2022*

Dear Water Warriors,

TDS transfer from water (Feed) into water (Reject) is an interesting water treatment technology, where we concentrate the impurities in small quantity of water making rest of the water free of TDS.

Reverse Osmosis is in in every process scheme these days and we use software to design and optimize the right RO system.



This issue of '**Waughter**', we requested SSr to design a plant for us and explain the way he thinks.

Let's design together.

Nidhi Jain – Civil Engineer

Defining the Input Required for RO Design?

In order to design a good RO system, one must have all the data mentioned in below table:

Sr No	Description		
1.01	Treated Water Quantity	m³/d	600
1.02	RO Operating hours	h	24
1.03	Permeate Flow Rate	m³/h	25
1.04	Feed Water Source		Borewell
	Feed Water Quality		
2.01	TDS	mg/l	2310
2.02	Conductivity	μS/Cm	3513
2.03	рН	-	7.8
2.04	TSS	mg/l	12
2.05	Turbidity	mg/l	6
2.06	Hardness	mg/l as CaCO3	250
2.07	Ca Hardness	mg/l as CaCO3	150
2.08	Mg Hardness	mg/l as CaCO3	100
2.09	Na+K	mg/l	By Calculation
2.10	Chloride	mg/l as Cl	700
2.11	Sulphate	mg/l as SO4	135
2.12	Nitrate	mg/l as NO3	12
2.13	M-Alkalinity	mg/l as CaCO3	210
2.14	P-Alkalinity	mg/l as CaCO3	0
2.15	Phosphate	mg/l as PO4	1
2.16	Boron	mg/l as B	0.1
2.17	Reactive Silica	mg/l as SiO2	23
2.18	F,NH4,Ba,Sr etc	mg/l as Such	If Available
	Treated Water Quality		
3.01	TDS	mg/l	100
3.02	Hardness	mg/l as CaCO3	10
3.03	Reactive Silica	mg/l as SiO2	1

Down the Memory Lane.. IMS Design

Was the First software Sanjeev Srivastava our Lead Technology ever used. Over the years many other software and Knowledge Partners also contributed to improving design thinking: Dupont, Dow, Suez, Toray, CSM, these names became synonym to Reverse Osmosis Know how and all are good.





He still remembers his first design, that was done through complicated Integral Calculus method manually without software. Unfortunately, he does not have hand notes of that and has forgotten manual calculations now.

Before you design.. with us together!

For the given data if you wish to design together for better learning. Please:

- 1. Read Waughter Volume 1 Edition 7
- 2. Download IMS Design on your computer

Once down you will reach the WINDOW as shown below

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Now follow magazine and software together.



Pure**COD**e

COD REDUCTION MEDIA

PureCODe is an absorbent media for the **lowering of recalcitrant COD** (Fine polishing of tough to treat COD) which subsequently helps in meeting stringent discharge norms in various industries such as textiles, chemicals, pharmaceuticals, etc. **This media is also regenerable on-site**.



PureCODe specialty media - helps in lowering COD significantly to meet stringent discharge norms and recycle maximum amout of water.

WORKING PRINCIPLES OF THE MEDIA:







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Feed Data into Software

When we enter the data available to us, the software suggested see below: (Warning! 81% Difference in Ions). This is because Na + K is not yet entered.



We need to Click on Na to adjust the same.

For TDS balance designer need to increase the Cl Value as well as Na value to reach design TDS of 2310 mg/l.

It is better to have 20% extra margin wrt to TDS. Remember Osmotic Pressure is directly proportional to the Feed TDS and thus 20% over design over design value is a good practice in designing RO system.

			23		
	mg/l	mg/l CaCO3		mg/l	mg/l CaCO
Ca	60.00	150.00	HC03	256.20	210.00
Mg	24.40	100.00	504	135.00	140.63
Na	921.95	2004.23	CI	1340.00	1889.99
к	0.00	0.00	F	0.00	0.00
NH4	0.00	0.00	NO3	12.00	9.68
Ba	0.000	0.00	P04	1.00	1.58
Sr	0.000	0.00	5102	23.00	
			1.00		
			В	0.10	
Total,	<u>meq/l</u>	45.08	B Total,	0.10	45.09
Total, Saturatio	meq/l	45.08	B Total,	0.10	45.09
Total, Saturatio Calculated 1	meq/l ons	45.08 2775 n g/l	B Total,	0.10 meg/l Ca504	45.09
Total, Saturatio Calculated 1 Osmotic pre	mea/l ons ros	45.08 2775 ng/l 2.0 bar	B Total,	0.10 <u>meq/l</u> CaSO4 BaSO4	45.05
Total, Saturatio Calculated 1 Osmotic pre Ca3(P04)2 :	meq/l ons ros	45.08 2775 n g/l 2.0 bar 0.29	B	0.10 meq/l CaSO4 BaSO4 SrSO4	45.09 1.1 % 0.0 %

Press Save As above Analysis Save and Continue...

Temperature is an important no in design (25 deg C), at higher temperature Feed Pressure reduced and quality deteriorates and vice versa.

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Analysis Design Calculation Post Treatment	
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Project: Waughter Vol 2 Edi 6 Calculated by: Vrushika Parmar Temperature: 25.0 🗠 Water Type: Brackish Well Non-Fouling Date: 7/1/2022	
	0 0
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K 0.00 0.00 F 0.00 0.00	0
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Landier ST 0.3 Siller 1.5 %	
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Design the RO system?

For a proper design we have several steps that need attention, let's move 1 by 1 to all steps and understand the significance of each.

Step 1

<u>Understand Feed Water</u>. For TDS up-to 8000 mg/l safely take Brackish Water RO membranes and above 22000 mg/l Sea Water RO membranes.

Selection of membrane also depends upon treated water quality. For stringent quality, you may have to select High Rejection membrane. (Feed Already Entered in previous Page)

Step 2

<u>Define Recovery</u>. One would like to go for highest recovery. High Recovery means less volume on Reject or more concentrated Reject. That means:

- a. Higher Osmotic Pressure barrier and hence high Feed Pressure.
- b. Solubility Concerns of Ca*HCO₃ and SiO₂
- c. Long Train of RO elements, remember 1st element recovers max 15% and next 15% from the balance 85% and so on...

The point c above defines no of stages. Since we have 6 Element long Pressure Tube, beyond 6 Serial no of stages increase. Let's design for 75% Recovery, i.e. 2 stages.

System Recovery	No of Elements in Series	No of Stages
40-60	6	1
60-80	12	2
80-94	18	3

Step 3

<u>Element Diameter</u>. Membranes are available in dia 2.5", 4" & 8". Generally, for flow rate < 200 lph we use 2.5" element and flow > 3 m³/h we use 8" element. In between it's better to use 4" element.

For special reasons or if low recovery is acceptable e.g. RO plants on boats, designer may use 8" membrane even at lower flow rates.

Step 4

<u>Flux Selection</u>. Flux means productivity of membrane per m² of its surface used for Filtration of clean water. Naturally it depends upon the amount (concentration) of unwanted materials. SDI usually is the measure of presence of impurities before the water is Fed to Reverse osmosis element. A sample of Flux guidelines is attached (All Membrane Suppliers issue such guidelines in their software):



In our case let's take Borewell water treated with conventional sand filter and select the flux as 28 l/m².h (range 27 -34 l/m².h)

Step 5

<u>Membrane Area Calculation</u>. Since we have flow rate as $25 \text{ m}^3/\text{h}$ and we have selected flux as 28 l/m^2 .h, her membrane Area required for our design is:

Membrane Area = Flow \div Flux = 25000 lph \div 28 l/m².h = 892 m² = 9607 ft²

So, our design shall have X Nos of membrane with Y ${\rm ft}^2$ surface each membrane

and X.Y = 9607 ft^2





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Step 6

<u>Membrane Selection</u>. In step 3 we understand 8" dia membrane is good for our design since flow rate is 25 m3/h.

BW elements (365 ft ²	3)	10
BW elements (400 ft	² and 440 ft ²)	10
NF elements		10
Full-fit elements		25
SW elements		10
	Active area	
Element type	ft ² (m ²)	
BW elements	365 (33.9)	65
BW or NF elements	400 (37.2)	75
BW elements	440 (40.9)	75
Full-fit elements	390 (36.2)	85
SW elements	320 (29.7)	65
SW elements	380 (35.3)	72
1 MF: Microfiltration - co	ntinuous filtration	1 pro
² The maximum recomm value is more limiting.	nended pressure We recommend	drop desi
Note: The limiting value quidelines results	s listed above ha in a warning on t	ve b he R

Close look of chart in Step 4 above suggests we have different elements with different active surface area. So let consider the membrane with Active Area of ~ 365 ft2

So our Nos of membranes required shall be

= 9607 ÷ 365 = 26.32 ~ say 27

Step 7

<u>RO Pressure Tubes</u>. The 27 Nos membrane calculated above need to be put into pressure tubes. The standard length of the tubes are 1,2,3,4,5 & 6.

Further in Step 2 we understand the Nos of stage shall be 2. i.e. Reject of Stage 1 shall be Fed to Stage 2.

If we select 6 Element Pressure Tube, we will need 6*5 = 30 membranes to fill all pressure tubes. If we select 5 Element Tube then we will need 5*6 = 30 membranes to fill all pressure Tubes.

In short Total no of membranes used ÷ No of Elements in Tube shall be a whole number. Let's select the Pressure Tube length as 5 El Long, means 6 Pressure Tube. Like below:



6 * 5 = 30 membranes filled in 6 Pressure Tubes that are each 5 El long.

Step 8

<u>Staging Ratio</u>. No of stages we selected depends upon recovery and for 75% we selected 2. The last stage shall always have $\frac{1}{2}$ the element of previous stage. So for a two stage system:

No of membranes in last stage $(2^{nd}) = A$ No of membranes in previous stage $(1^{st}) = 2A$



Thus 3A = 30 and A = 10. So our Staging would be as shown above. Here one can say that ~ 50% recovery is achieved in stage 1 and 50% of 50% balance that is ~ 25% is recovered is stage 2 making overall recovery as ~ 75%.

Final 25% is reject water that is removing TDS that has been rejected by membrane.

Step 9

For 9th step, we need to understand the word "Integral Calculations", Look at below Pressure Tube and understand what's happening when water is flowing:



- a. Feed Flow is decreasing and becomes 5 m³/h at end as some of it becomes permeate.
- Osmotic Pressure keeps increasing as TDS becomes 1950 from starting 1000 mg/l
- c. Since Feed Pressure say ~ 12 kg/Cm², will keep reducing, NDP (Nett Drive Pressure = Feed Pr Osmotic Pr) will decrease.
- d. Thus, the Permeate production shall decrease as we travel down the tube means 1st element will produce most of the permeate and last the least.
- e. Bottom line: Flux is always reducing.

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Step 10

<u>Software Use</u>. The design obtained from above 9 steps is transported on a software to perform calculations and check if the guidelines for membrane use are violated. One must balance the flow (Flux) to ensure:

- a. Lead Element flux is not higher than the limit set.
- b. Brine leaving from last element should not be lower than defined value, else scaling/fouling. Minimum Sweep velocity to be maintained.
- c. Make better use (Flux) of tail end elements
- d. Many more reasons as we learn along

Our design as entered in software shall look as in below figures.

- A. Press Run to check if design is OK, the calculations are performed and we have:
 - 1. Beta High 1.21 marked in Red
 - TDS < 63 mg/l as per our design.

alcu	lation R	esults	5					(6	lows are per vessel	
Arra	ry Vei	sels	Feed (bar)	Conc (bar)	Feed (m3/h)	Conc (m3/h)	Flux (lmh)	Highest flux: (lmh)	Highest bets	
1-1	6	4	12.8	11.	9 8.33	3.36	29.4	34.3	1.21	
1-2	2	2	11.7	1	1 6.71	4.16 1		20.0	1.10	
	cure com									
Ca [0.028	κ	0.000	Sr	0.000 d	27,619	P04 0.0	05 002	5,420	
Ca C	0.028	K NH4	0.000	Sr HC03	0,000 CI	27.619 1.747	PO4 0.0	05 CO2	5,420	
Ca Mg Na	0.028	K NH4 Ba	0.000	Sr HC03 504	0.000 Cl 9.434 NO3 0.701 F	27.619 1.747 0.000	P04 0.0 102 0.4 8 0.0	05 CO2 04 CO3 83 pH	5,420 0,001 6,4	

To correct Beta, reduce recovery and enter correct membrane age as 3 years, we get final design as:

the second s			Pass 1				Pass 1	
Feed pH		-	7.80		Chemical		H2504	•
Permeste re	covery	5	73.00		Solution concent	tration, %	100	÷
Permeste flow/train. m3/h Average flux Imh		m3/h •	25.00		Chemical dosing rate	mp/l	. 0.0	00
		mh 24.5			Membrane age.	vears	3	3.0
Feed flow, m3/h		m3/h	34.25	i.	Flux decline %.	pervear	5.	00
Reject flow		m3/h	0.00				0.0	57
alare upon			9.25		Fouling factor		0.0.	3/
Calculatio	on Result	5	9.25		Fouling Factor SP increase % p	er year	(7)	она are per v
Rafculatio	on Result Vessels	5 Feed (bar)	Gonc (bar)	Feed (m3/h)	Fouling factor SP increase % pi Conc (m3/h)	er year Flux (imh)	(5 Highest flux (Imh)	10 Highest Highest
Raiculatii Array 1-1	on Result Vessels	5 Feed (bar) 13.9	9.25 Conc (bar) 12.9	Feed (m3/h) 8.56	Conc (m3/h) 3.74	er year Flux (lmh) 28.5	(F Highest flux (Imh) 32.4	Highest beta

The Screen shot of data entry, please mark membrane age 0 is a wrong entry it must be 3.

- Concentrate Recirculation is a way to increase recovery and control Beta Factor (Higher flow from lead element)
- Booster Pump design is to ensure better flux distribution through-out membrane train and energy optimization
- Permeate Back Pressure design controls higher flow from lead elements. Can pose engineering challenge while construction, be careful.

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Save As T Conc. Recirculation Rootter Pump	▼ Calculator
Project file Options Actions	Two Pass Tools
Project: Waughter Vol 2 Edi 6 Calculated by: Vrushika Parmar Temperature: 25.0 🗠 Water Type:	Brackish Well Non-Fouling Date: 7/1/2022
Trains best	Sustan
Fact all 2 mail Chemical H2001 +	
Permeate recovery % 75.00 Solution concentration.% 100 *	Number of Traina
Permeate Bow/train. m3/h + 25.00 Chemical dosing mg/l + 0.000	
Average flux Imh 24.5 Membrane age, years 0.0	0 0 0
Feed flow. m3/h 33.33 Flux decline %. R#F.x##F. 5.00	000
Reject flow m3/h 8.33 Fouling factor 1.00	0
SP Increase % per year 7.0	
	1 Floating Diagram
System Specification	
State 1 State 2	
Element type CPA2 CPA2 Stages 2.	
Elements / Vessel 5 5 Pass 1 2	
No. of Vessels 4 4 Recalc array	
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Final Design

The Final design thus has 73% recovery, TDS < 70 mg/l and designer can take a complete 3 page print to see the design and performance of each element.



The PDF of 1st page of design is of interest wrt to solubility points:

Created	un: 7/1/20	22 03 59:4	0								Vitto		the Okramyo Con	many and
							Ba	sic Desig	jn i					1
Project	name			Nauchter	Vol 2 F	di di								Ent : 1/3
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Feed te	mperatur					25	0 °C(77	(0°F)	Element :	100			3.0 v	ears
Feed w	ater oH					7.	80		Flux decil	no %, per v	ear		5.0	100
Chem d	tose, mp/	L-				H250	04	. 1	Fouling fa	ctor			0.86	
Specific	c energy					0.	05 kwh/r	n3	SP increa	se, per yea	I :		7.0	16
Pass NI	DP					5	1.5 bar		Inter-stag	e pipe loss			0.207 b	ar
Average	e flux rate	11				24	15 Inh							
								-	Feed type			Brackish We	Il Non-Fouli	ng
Pass -	Perm.	Flow /	Vessel	Flux	DP	Flux	Beta	Stag	ewise Pro	essure	Permu	Element	Element	PV₽ x
Stage	Flow	Feed	Conc			Max		Perm.	Boost	Cono	TDB	Туре	Quartity	Elem #
	m3h	m3/h	m3/h	Imb	bar	Imh		bar	bar	bar	mgil			
1-1	19.3	8.6	3.7	28.5	0.9	32.4	1.19	0	0	12.9	41.9	CPA2	20	4 x 5M
1-2	5.7	7.5	4.6	17	0.9	21	1.1	0	0	11.9	164	CPA2	10	2 x 5M
Ion (mp)	0					Row V	later	Feed Wate	r Pern	cote Water	Concentrate 1	Concentrate	2	
Hardnes	is, as CaCi	38					250.00	25	1.00	0.130	572.3	9	27.7	
Ca							60.00	6	1.00	0.031	137.4	2	22.6	
Ng							24,40	20	1.40	0.013	20.9		00.5	
ĸ							0.00		1.00	0.000	0.0		0.0	
14-14							0.00		1.00	0.000	0.0		0.0	
Ba							0.000	0	000	0.000	0.0		0.0	
Br							0.000	Ó	000	0.000	0.0		0.0	
H							0.00		1.00	0.000	0.0		0.0	
HODI							256.20	26	1.20	10.525	500.0		20.2	
504							135.00	13	5.00	0.786	308.5	4	0.00	
C							340.00	1341	1.00	30.965	3044.1	48	90.5	
F							0.00		1.00	0.000	0.0		0.0	
NO3							12.00	1	2.00	1.946	25.9		29.3	
OH					-		0.01		105	0.006	23		0.0	
5002							23.00	2	3.00	0.452	12.3		64.2	
в							0.10	1	0.10	0.089	0.1		0.1	
002							5.42		5.42	5.42	5.42		5.42	
NH3						100	0.00	1	1.00	0.00	0.00		0.00	
pH							7.80	200	7.89	6.48	6.12	1010	8.29	
Satura	tions					0	Dam West	and the second se	Food	Water	Conren	trate	Limi	br.
CHSCH	L/km* 1	00 %					1		2000	1	B		AD	1
SrSO4	/ksp * 10	0. %					0			0	0		120	0
BaSO4	/ksp*1	00. %					0			0	0		1000	00
SiO2 84	aturation.	%					17		63	17	55		140)
CaF2/	ksp * 100	1, 95					0			0	0		5000	00
Ca3(Pt	O4)2 satu	ration ind	(entr.				0.3		1	2.3	1.4		2.4	ē.
COPP.	mgil						14.01		14	101	283.6	34	850	0
Langei	ier satura	ton index	£				0.27		0	27	1.81		2.8	6
Ionic st	trength						0.05		0	.06	0.18	3		
Osmot	ic pressur	e, bar					2.0		1	2.0	7.4			

The LSI of 1.8 indicates we need to add antiscalant.

Further SiO₂ saturation is in in limit so no worries, or else use antiscalant till SiO₂ in Concentrate 2 is up to 300 mg/l

For more practice and perfect your design.

जल जीवन जननी !!



Our world is Waughter

The technical knowledge share attempt of Aktion Consultancy and the contents in the magazine shall be qualified by Sanjeev Srivastava our Technology Lead.

Our next edition focuses on: "UF Design & BOQ Generation"

Please feel free to write or contact Mrs. Neha Deshpande 95129 55227

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